

Mechanics of CEPC Magnet and Calorimeter

Pei Yatian

On behalf of CEPC Magnet, HCAL and ECAL group

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中國科學院為能物昭和完備 Institute of High Energy Physics Chinese Academy of Sciences

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Outline

Overview of Magnet, HCAL and ECAL structure

- Technical design of Magnet
 - Detailed design of the detector magnet
 - Simulation of coil
 - Cryogenic system and cryostat
 - R&D and prototypes

Mechanical design of HCAL

- HCAL mechanics design
- HCAL cooling system

Mechanical design of ECAL

- ECAL mechanics design
- ECAL cooling system
- Next plan

Overview of Magnet, HCAL and ECAL structure





Magnet

- Large-size and high-strength Aluminum stabilized superconducting cable;
- Suspension system of the huge coil (145 tons);
- High precision machining and assembly of large scale coil;
- There are lots of welds in low-temperature pipes, including pipes and coil supports, pipes and liquid/gas helium tanks.



Detailed design of the detector magnet Main parameters of Magnet



- Red color is Yoke and its weight is 2960 tons
- Black border line is Magnet and its weight is 250 tons
- Purple color is coil and its weight is 145 tons

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00	Parameter Value		Barrel parameter	Value
	Inner diameter	7070 mm	Inner inradius diameter	8490mm
	Outer diameter	8470 mm	Outer inradius diameter	10370mm
	Length	9050 mm	Length of barrel	9150 mm
	J Main parameter	rs of coil	Quantity of layer	7
Parameter Value		Gap between two layers	40mm	
Coil Inner diameter 7300 mm		7300 mm	Weight	1560tons
Coil Outer diameter 7916 mm		End-cap parameter	Value	
Coil	length	8150 mm	Inner diameter	1300mm
Cen	tral magnetic field	3 T	Outer inradius diameter	10370mm
Ope	rating current	17 kA	Thickness of one end	1240mm
Coil	Module gap	50 mm	Quantity of layer	7
Inductance 11 H		Gap between two lavers	40mm	
nut		±± 11		

□ Main parameters of Yoke



• Detailed structure of magnet



Table 10.3: Conductor overall characteristics

Parameters	Value
Nominal design current	17 kA
Critical current at 4.2 K and 5 Tesla	51 kA
Total length of conductor	33 km
Overall dimension (Without Insulation)	$56 \text{ mm} \times 22 \text{ mm}$
Superconducting cable cross section area	$2.2 \text{ mm} \times 20.5 \text{ mm}$
Al stabilizer cross section area	$12 \text{ mm} \times 40 \text{ mm}$

Simulation of coil

The magnetic induction intensity at the point of interaction on the axis is 3 T, and the peak field on the coil is 3.8 T



Overall distortion of the coil

The coil mainly faces two working conditions: cooling to 4.2 K and excitation to 17 kA.

During the actual installation of the coil, deviations from the design position are inevitable due to processing and measurement errors

Material Vo	Von Mises stress(MPa) Allowable stress(MPa)				
Coil at 4.2K (After cooling)					
Aluminum stabilizer	7.7-20.0	65	34		
NbTi/Cu cable	177-279	PASS	>800		
Al alloy	7.0-43.3		>500 (160)		
Al alloy support	6.3-36.3		>500 (160)		
Coil at 4.2K (After exciting)					
Aluminum stabilizer	14.3-22.5	(S)	34		
NbTi/Cu cable	28-246	PAS	>800		
Al alloy	60.8-137		>500 (160)		
Al alloy support	62.2-127		>500 (160)		
Table	Table 10.7: Forces and torques of coil offset				
Axial displacement (cm)	1	3	10		
Axial force (kN)	391	1247	5276		
Radial displacement (cm)	1	3	10		
Radial force (kN)	49.3	258	708		
Angular tilt (degree)	$1/407.5 = 0.14^{\circ}$	$3/407.5 = 0.42^{\circ}$	$10/407.5 = 1.41^{\circ}$		
Torque $(kN \cdot m)$	1678	7020	17647		

Cryogenic system and cryostat

Cooling methods: Thermal siphon

	Thermal siphon	Forced flow
Difference	Need more space to install the phase separator	A liquid helium circulating pump is required
Heat exchange capability	1200 W/(K·m²)	412.1 W/(K⋅m²)
Coil maximum temperature	4.982 K	5.383 K
Coil average temperature	4.591 K	4.972 K
Size of Liquid helium pipes	Φ15 mm	Φ 20 mm



A 4 K liquid helium cryogenic system

The coil cryogenic system within the coil vacuum vessel
 The compressor and refrigerator (including liquid helium Dewar)
 The cryogenic transfer and distribution system (valve box and piping)

④ The recovery and purification system.

Heat loads calculation

Table 10.13: The heat load of 4K

Component	Heat Load (W)
Static heat loads	157
Peak value of dynamic heat load	193
Total	350

 Table 10.14:
 The heat load of 60 K thermal shield

Component	Heat Load (W)
Radiation heat load	373
Support heat load	54
Phase separator / Pipes / Valves	160
Current leads	2000
Dynamic heat loads	65
Total	2652

Cryogenic system and cryostat

Temperature distribution result by FEA

Coil cryogenic circuits





Cryogenic system and cryostat



Suspension system



Table 10.18: Parameters of the titanium alloy rods. There are three types of rods used in the coil suspension system. Different rods have different functions.

Rod Type	Diameter (mm)	Length (mm)	Screw
Axial rods	30	3530	M36×3
Radial rods	40	1700	M48×4
Main pull rods	48	1650	M56×4

Cryogenic system and cryostat

Vacuum tank



Figure 10.59: Deformation distribution of the vacuum tank



Figure 10.60: Stress distribution of the vacuum tank

Magnet support system



Figure 10.64: Final connection structure

 Table 10.21: Deformation and stress of support structure under different coil offset conditions

Parameter	1 cm	3 cm	10 cm	
Axial d	isplaceme	ent		
Deformation (mm)	0.0556	0.0559	0.0568	
Stress (MPa)	391	394	402	
Radial displacement				
Deformation (mm)	0.056	0.057	0.059	
Stress (MPa)	392	398	416	
Ang	gular tilt			
Angular tilt (degrees)	0.14	0.42	1.41	
Deformation (mm)	0.064	0.025	0.062	
Stress (MPa)	423	1308	3201	

R&D and prototypes

Conductor R&D and prototypes



Stranding process

Table 10.8: SC strands parameters

Parameters for wires	Value
Strand diameter	1.30±0.01 mm
Cu/SC ratio	$1.07 \pm 10\%$
Ic @5 T,4.2 K	1750 A
RRR of copper matrix	100
Filament diameter	About $34\mu m$
Number of filaments	708

First and second co-extrusion forming

A 3m long sample conductor with box configuration superconductor

- Before and after stranding, the NbTi wire's critical current decay is less than 5%, and the RRR value of copper declined by about 1/3 after the stranding process.
- After second co-extrusion process, the critical current decay is bout 10%
- A first 16 strands Aluminum stabilized superconductor was realized as the R&D (In the future it is 32 strands).
 - I The shear strength between aluminum and Rutherford cable is 35 MPa

R&D and prototypes

Dummy coil development



Figure 10.12: The diagram of the winding line

- Mainly includes cable drum, straightening machine, buffering support frame, winding forming machine, rotary platform, and winding mold
- Using the inner winding technique and vacuum impregnation of large-diameter coils
- The dummy coil consists of an aluminum alloy support cylinder and 4 layers of coils, with 10 turns per layer



HCAL

- The space for mechanics and services (e.g. cooling, cabling) integration is very narrow;
- Supporting structure need to ensure mechanical stability and alignment precision throughout the detector's lifetime. Which means how can we use 46% weight to support 54% weight.





Layout for all the HCAL components



D Requirements:

- \bullet The support structure zone is as lower as possible.
- The maximum stress of different materials need to be lower than their allowable stress level.
- The deformation of different materials need to be controlled so that there will be no broken parts under different conditions.
- Outer contour dimension tolerance need to be 0mm to -5mm and inner contour dimension tolerance need to be 0mm to +5mm.

General structure information:

- The cross section of HCAL is a regular hexadecagon
- Total weight is 1679 tons and there are totally 5224960 glass scintillator

Layout of one detect module



40mm

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Connection structure of barrel HCAL

Edge sealings



FEA result

Stress and deformation of barrel HCAL under different conditions Deformation Stress **Parameter** 24.7MPa 0.33mm One wedge assembling condition 190MPa 0.66mm 16 wedges assembling condition Barrel ECAL connection condition 1.26mm 1.264 1.1225 0.9601 0.84266 0.76222 0.56177 0.42133 0.26089 0.14048 **Boundary** condition 3/yee Equations Use: MPa Tree 1 Mar: 371.1 Mar: 90771e-10 2025/3/9 11.92 386.63 247.4 386.61 164.90 123.7 02.665 41.233 9.0776-10 Changing the 371.1MPa trapezoid beam from stainless steel to titanium alloy

Active layer space analysis Total Deformation 4 Type: Total Deformatio Unit: mm Time: 1 Max: 1.2455 Min: 1.0473 2025/3/3 12:5 The deformation difference between 48 layer is 12455 1.2235 1.2015 1.1794 1.1574 lower than 0.2mm 1.1354 1.1134 1.0914 1.0694 The deformation of all 48 layers at the same X D: Copy of Copy of Copy of Cop Total Deformation 5 Type: Total Defor Unit: mm Time: 1 The difference between the lowest point to highest Max: 1.2078 Min: 0.70305 2025/3/3 13:08 point is 0.5mm 1 2078 1.1517 1.0956 1.0395 0.98346 0.92738 0.87129 0.81521 0.75913 Deformation within one layer GS analysis A: Static Structura A: Static Structural Total Deformation **0.5mm** Maximum Principal Stress 2 **20MPa** Type: Total Deformation Type: Maximum Principal Stress Unit: mm Unit: MPa Time: 1 2025/3/3 13:21 2025/3/3 13:22 0.5008 Ma: 20.087 Max 0.44515 17.628 0.38951 15,168 0.33387 12,709 0.27822 0.22258 10.25 0.16693 7.7903 5.331 0.11129 0.055644 2.8717 0.41235 -2.047 Mir







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HCAL cooling system

Cooling scheme definition

Ambient temperature: 25 °C



 $T_{max} = 39.95 \,^{\circ}\text{C}, \, T_{min} = 36.43 \,^{\circ}\text{C}$

FEA result of thermal performance of natural convection Ambient temperature: $25 \circ C$, $V_{in} = 1 \text{ m/s}$



 T_{max} = 28.23 °C, T_{min} = 25.02 °C FEA result of thermal performance of air-cooling

The temperature error of different SiPM need to be controlled less than \pm 1.5°C

- The excessively narrow interlayer gaps significantly reduce the efficiency of natural convection and air cooling, thereby failing to address the thermal management demands.
- It is imperative to adopt liquid cooling technology to ensure efficient heat dissipation and temperature uniformity.

Cooling structure of barrel and end cap HCAL







- 4/3 pipes in each layer in parallel
- 8 layers gather in one pipe in parallel
- One end is inlet and another end is outlet
- 1 pipe in each layer
- 5 layers gather in one pipe in parallel
- 16 wedges, with each region having one inlet and outlet.

HCAL cooling system

FEA simulation of cooling system

$T_{max} = 15.56 \ ^{\circ}\text{C}, \ T_{min} = 15.00 \ ^{\circ}\text{C}$



Temperature distribution of the HCAL through liquid cooling

- ♦ Inlet temperature is 15 °C with a flow rate of 0.005 kg/s (corresponding to an inlet velocity of 0.1 m/s).
- Effectively maintaining the temperature rise below 0.6 ° C.
- The maximum temperature variations of chips under the same box were under 0.1 ° C

- (a) Eight-in-one design of flow pipe
- (b) Flow velocity distribution across different layers
- Achieving a uniform flow velocity distribution across different layers
- The pipe resistance and length of endcap HCAL is smaller than barrel HCAL, so the same scheme can also meet our requirement
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ECAL

 The calorimeter design must be hermetic, meaning minimum space for mechanics and services (e.g. cooling, cabling) integration;
 Large-size carbon fiber structure processing
 High precision manufacturing and assembling;





Layout for all the ECAL components



General structure information:

- ◆ The transverse cross-section of the barrel ECAL is defined as a 32-sided polygon
- ◆ Total weight is **180 tons** and there are totally **about 210000 BGO**

D Requirements:

- Minimize the material volume of the support structure to reduce passive material within the sensitive volume.
- Ensure that maximum stress in each component remains below the respective material's yield strength.
- Deformations of different materials must be controlled to prevent structural failure under varying operating conditions.
- Maintain outer contour dimension tolerances within [0, -5] mm and inner contour tolerances within [0, +5] mm.



Barrel ECAL mechanics

Integration of barrel HCAL structure



- In each segment: two crystal modules in trapezoid-shape
- Main structure is based on carbon fibers



Connection structure of barrel ECAL

Interfaces between crystal module and CFRP frame



Interfaces between crystal module, cable and cooling pipe



The smaller end is positioned and supported by the frame itself, while the larger end is secured using mechanical stoppers to prevent module slippage. These stoppers are fastened to the frame with screws and further reinforced with structural adhesive.

Eight uniformly distributed suspension fixtures

Endcap ECAL mechanics

Integration of barrel HCAL structure

- 32 segments in phi
- Total of six types of modules

Main structure is based on carbon fibers

• Crystal granularity: $15 \times 15 \text{ mm}^2$





16 fixation points are added in the central region within the gaps between the ECAL and HCAL



Old version

-31.4523 31.4523

20.166 203.071

157.262

FEA result of endcap ECAL composite frame



Trapezoidal crystal detection modulesin the barrel ECAL is identical to thatused in the endcap ECAL

Deformation and Stress in Various Directions of the Composite Frame Under Self-Weight and External Load

ECAL cooling system

FEA simulation of cooling system

Requirements:

- Inlet cooling water temperature of 15.C
- Maximum operating temperature need to below 25.C.

Endcap ECAL is almost same with barrel ECAL



 Table 7.9:
 Temperature rise of cooling water.

Parameter	Single Module Rise	Cumulative Rise (15 Modules)	Final Inlet Temperature
Cooling Water	0.13 (°C)	1.95 (°C)	16.95 (°C)

Next plan

Magnet

- High strength and high RRR value aluminum stabilizer research.(2025)
- Full size Aluminum stabilized superconducting cable development. (2025)
- Detailed design of mechanical system. Optimize the thickness design of magnet.(2026)
- Validation experiments for mechanical and cryogenic systems.(2027)

HCAL mechanics

- To further optimize GS-SiPM coupling, cooling scheme
- To further optimize the support structure
- To prepare full-size GS-HCAL prototype for beam test

ECAL mechanics

- Optimizing the CF structure
- FEA crosschecks, CF structure production vendors (wider survey)
- Full-scale crystal calorimeter prototype and beam tests: integrated with mechanics/cooling

Thanks